

Electrically Conductive Non-Aqueous Wellbore Fluids

This invention relates to non-aqueous wellbore fluids and in particular concerns wellbore fluids which are electrically conductive. The invention also relates to the use of said wellbore fluids for drilling fluids or completing fluids for subterranean wells such as for instance oil and gas wells.

In the process of rotary drilling a well, a drilling fluid or mud is circulated down the rotating drill pipe, through the bit, and up the annular space between the pipe and the formation or steel casing, to the surface. The drilling fluid performs different functions such as removal of cuttings from the bottom of the hole to the surface, to suspend cuttings and weighting material when the circulation is interrupted, control subsurface pressure, isolate the fluids from the formation by providing sufficient hydrostatic pressure to prevent the ingress of formation fluids into the wellbore, cool and lubricate the drill string and bit, maximise penetration rate etc. An important objective in drilling a well is also to secure the maximum amount of information about the type of formations being penetrated and the type of fluids or gases in the formation. This information is obtained by analysing the cuttings and by electrical logging technology and by the use of various downhole logging techniques, including electrical measurements.

The required functions can be achieved by a wide range of fluids composed of various combinations of solids, liquids and gases and classified according to the constitution of the continuous phase mainly in two groupings : aqueous (water-based) drilling fluids, and non-aqueous (mineral oil or synthetic-base) drilling fluids, commonly ' oil-base fluids'.

Water-based fluids constitute the most commonly used drilling fluid type. The aqueous phase is made of fresh water or, more often, of a brine. As discontinuous phase, they may contain gases, water-immiscible fluids such as diesel oil to form an oil-in-water emulsion and solids including clays and weighting material such as barite. The properties are typically controlled by the addition of clay minerals, polymers and surfactants.

In drilling water-sensitive zones such as reactive shales, production formations or where bottom hole temperature conditions are severe or where corrosion is a major problem, oil-based drilling fluids are preferred. The continuous phase is a mineral or synthetic oil and

commonly contains water or brine as discontinuous phase to form a water-in-oil emulsion or invert emulsion. The solid phase is essentially similar to that of water-based fluids and these fluids too contain several additives for the control of density, rheology and fluid loss. The invert emulsion is formed and stabilised with the aid of one or more specially selected emulsifiers.

Although oil-based drilling fluids are more expensive than water-based muds, it is on the basis of the added operational advantage and superior technical performance of the oil-based fluids that these are often used for the drilling operations.

An area where oil-based muds have been at a technical disadvantage, because of their very low electrical conductivity, is in electrical well-logging. Various logging and imaging operations are performed during the drilling operation, for example while drilling in the reservoir region of an oil/gas well in order to determine the type of formation and the material therein. Such information may be used to optimally locate the pay zone, i.e. where the reservoir is perforated in order to allow the inflow of hydrocarbons to the wellbore.

Some logging tools work on the basis of a resistivity contrast between the fluid in the wellbore (drilling fluid) and that already in the formation. These are known as resistivity logging tools. Briefly, alternating current flows through the formation between two electrodes. Thus, the fluids in the path of the electric current are the formation fluids and the fluid which has penetrated the formation by way of filtration. The filtercake and filtrate result from filtration of the mud over a permeable medium (such as formation rock) under differential pressure.

Another example where fluid conductivity plays an important part in the drilling operation is in directional drilling where signals produced at the drill assembly have to be transmitted through an electrically conductive medium to the control unit and/or mud telemetry unit further back on the drill string.

At present the use of resistivity logging tools is limited mainly to cases where a water-based drilling fluid is used for the drilling operation (the very low conductivity of the base-oil in the case of oil/synthetic-base muds precludes the use of resistivity tools in such fluids). Although the brine dispersed in the oil phase is electrically conductive, the discontinuous nature of the droplets prevents the flow of electricity. Indeed, the inability of these emulsions to conduct electricity (until a very high potential difference is applied) is used as a standard test of emulsion stability. To that extent it is worth bearing in mind that the

electrical conductivity k of the oil base is typically in the range 10^{-6} to $5 \times 10^{-2} \mu\text{S.m}^{-1}$ at a frequency of 1 kHz while an electrical conductivity of not less than $10 \mu\text{S.m}^{-1}$ and preferably of no less than $10^3 \mu\text{S.m}^{-1}$ is desirable for electrical logging operations. So there is a need to increase the electrical conductivity of the fluid by a factor in the order of 10^4 to 10^7 .

5 A few attempts to make oil-based drilling fluids electrically conductive for the purpose of electrical logging have been reported though none of them has been a commercial success. U.S. Patent No. 2,542,020, U.S. Patent No. 2,552,775, U.S. Patent No. 2,573,961, U.S. Patent No. 2,696,468 and U.S. Patent No. 2,739,120, all to Fischer, disclose soap-stabilised oil-based fluids comprising an alkaline-earth metal base dissolved in up to 10% by weight
10 water. Fischer claims to reduce the electrical resistivity to below 500 ohm-m which corresponds to an increase of conductivity to $\kappa > 2000 \mu\text{S m}^{-1}$. However, those fluids happen to be very sensitive to contaminants and greater amounts of water lead to unacceptable increase of the fluid loss. In essence these fluids relied on the residual or added water content to dissolve the salts/surfactants. Moreover, the continuous oil phase fails to exhibit any
15 increase of its electrical conductivity and there is no reference to what happens to the filtrate which under optimum conditions is made up essentially of the continuous oil phase.

Twenty five years later, U.S. Patent 4, 012,329 disclosed an oil-external micro-emulsion made with sodium petroleum sulfonate and reported of resistivity $< 1 \text{ ohm-m}$ ($\kappa > 1 \text{ S m}^{-1}$). In such a micro-emulsion, the sodium petroleum sulfonate forms micelles that contain water
20 and the clay so that the clay has to be added as a dispersion in water and cannot be added as dry powder. It should be also emphasised that a micro-emulsion is distinctly different from a standard emulsion, being thermodynamically stable, smaller in size, higher in surface to volume ratio and forming both filtercakes and fluid filtrate of a different nature. Obtaining the necessary combination of bulk properties and non-damaging rock interactions is more
25 difficult than for a standard direct or invert emulsion fluid, and such fluids are not generally favoured for drilling oil wells.

Although the Prior Art contains formulations for making oil-based drilling fluid conductive, the methods so described adversely affect other mud properties, another reason why none have been successfully commercialised. Further, the Prior Art only addresses the problem of
30 increasing the conductivity of the entire fluid but fails to teach any drilling fluid that exhibits a good conductivity of the oil phase making thus also a conductive filtrate which is free of solids and emulsion droplets.

The aim of this invention is thus to provide a wellbore fluid whose continuous phase is non-aqueous and exhibits an electrical conductivity well above the conductivity of organic liquids known to those skilled in the art to be suitable as the liquid phase of conventional non-aqueous based wellbore fluids.

- 5 To this end, the invention provides a wellbore fluid having a non-aqueous continuous phase comprising a polar organic liquid (POL) component that exhibits a dielectric constant of at least about 5.0, and preferably of at least 10, and a Hildebrand solubility parameter of at least about $17 \text{ (J cm}^{-3})^{1/2}$ at 20°C .

The Hildebrand solubility parameter δ is a measure of solvent power and is defined as the
10 square root of the cohesive energy density of a compound, that is the energy required to break the attractive forces between molecules of 1 cm^3 of material at a certain temperature T . This energy is related to the molar heat of vaporisation ΔH_m at this temperature, the work needed to expand the volume of the system from the liquid to the vapour phase RT and the molar volume of the solvent V_m according to the following formula : $\delta = \sqrt{\frac{\Delta H_m - RT}{V_m}}$ in

- 15 which R is the gas constant and T the temperature in $^\circ\text{K}$. When neglecting the RT term, the Hildebrand solubility parameter can be roughly expressed as the square root of the product of the density d and the heat of vaporisation ΔH ($\Delta H_m = \Delta H \times \text{molecular weight}$):
$$\delta = \sqrt{\Delta H \cdot d}$$

- 20 Said polar organic liquid POL component may be selected from the class including but not limited to alcohols, phenols, glycols, polyalkylene glycols, mono (alkyl or aryl) ethers of glycols, mono (alkyl or aryl) ethers of polyalkylene glycols, monoalkanoate esters of glycols, monoalkanoate esters of polyalkylene glycols, ketones possessing also hydroxyl group(s), diketones and polyketones.

- 25 The required dielectric and solubility properties can be also achieved with aprotic solvents such as ketones; nitriles; di(alkyl or aryl) ethers of polyalkylene glycols; dialkanoate esters of polyalkylene glycols; cyclic polyethers; N-(alkyl or cycloalkyl)-2-pyrrolidones, N-alkyl piperidones; N,N-dialkyl alkanoamides; N, N, N¹, N¹-tetra alkyl ureas; dialkylsulphoxides; pyridine and alkylpyridines; hexaalkylphosphoric triamides; 1,3-dimethyl-2-imidazolidinone, nitroalkanes, nitro-compounds of aromatic hydrocarbons, sulfolane, butyrolactone, and
30 propylene carbonate.

The polar organic liquid component that exhibits a dielectric constant of at least about 5 and a Hildebrand solubility of at least about $17 \text{ (J cm}^{-3})^{1/2}$ at 20°C may be used as part or all of the organic liquid phase of a wellbore fluid to substantially increase the electrical conductivity whilst maintaining the expected performance advantages of oil-based wellbore fluids.

Oils or other organic liquids known to be suitable as the continuous liquid phase of wellbore fluids, may be used in admixture with the POL component of this invention. This generally includes any water immiscible organic liquid (OL) known to those skilled in the art to be suitable as the liquid phase of non-aqueous based wellbore fluids (such liquids typically exhibiting electrical conductivity in the range 1.0×10^{-6} to $1.0 \times 10^{-2} \mu\text{S m}^{-1}$ at a frequency of 1 kHz).

It has further been found that certain inorganic salts, organic bases, quaternary ammonium salts or hydroxides (the dissolved component, DC), display sufficient solubility (and current carrying abilities) in POL, OL or in mixtures of liquid (POL) and liquid (OL), that the electrical conductivity of the mixture is greatly improved. Therefore, in this instance the use of liquid (POL) may not be necessary.

It is further found that when the polar organic liquid POL is used as part or all of the organic liquid, water can dissolve to some extent and increase electrical conductivity substantially.

Generally, the best results are obtained from a combination of (POL) and (DC), either alone or in admixture with (OL). In any case, the liquid phase is characterised by exhibiting an electrical conductivity of not less than $10 \mu\text{S m}^{-1}$. This is an increase of at least 10^4 fold over the conductivity of conventional organic liquids used as the wellbore fluid continuous phase. For convenience, any of the above combinations of (POL), (OL) and (DC) are designated hereafter as NBL (Novel Base Liquid).

Thus, the continuous liquid phase according to the present invention may be

- (i) entirely (POL)
- (ii) 1 to 99.9% by volume of (POL) + 99 to 0.1% by volume (OL)
- (iii) 50 to 99.5% by volume of (POL) + 50 to 0.5% by volume (DC)
- (iv) 50 to 99.5% by volume of (OL) + 50 to 0.5% by volume (DC)
- (v) 1 to 98.5% by volume (POL) + 1 to 98.5% by volume (OL) + 0.5 to 50% by volume (DC).

The liquid phase exhibits an electrical conductivity of not less than $10 \mu\text{S.m}^{-1}$ at 1 kHz.

The most important attribute of this invention is that the electrical conductivity of the fluid is increased by a factor of the order of 10^4 to 10^7 . This allows for the first time the successful application of many electrical logging techniques and the transmission of electrical telemetry signals when organic liquid-based wellbore fluids fill the borehole.

In this invention it has been found that for the first time electrically conductive, organic liquid-based drilling fluids can be provided which maintain the performance advantages expected from known oil-based (or synthetic organic liquid-based) drilling fluids. Therefore, the fluids of this invention minimise adverse interactions with drilled rock formation, such as clay formation swelling or dispersion, hole collapse, or the undesirable dissolution of underground salt formations. They also provide the performance advantages expected from oil-based fluids with regard to enhanced lubricity, reduced differential sticking of drill pipe, and good stability at high temperatures.

Optionally, as in conventional organic based wellbore fluids, a discontinuous liquid phase such as water or a brine may be added together with one or more emulsifiers to form a water-in-NBL emulsion wherein the discontinuous phase is present at up to 70% by volume of the emulsion.

The electrical conductivity of the wellbore fluid based on NBL, and that of its filter cake formed on permeable rock formations, may be further enhanced by dispersing in the wellbore fluid finely divided particles of an electrically conducting solid which is insoluble in the NBL or the water (or brine) phase. These particles may comprise of (but not be limited to) metals, carbon in the form of carbon fibre or graphite, metal coated carbon fibre or graphite, conductive polymers such as polypyrrole, polyaniline, or organometallic phthalocyanines. It is preferred that the solid particles are of very small particle size (in order not to be removed by solids control equipment), and exhibit an anisotropic particle shape such as needles, fibres, flakes or platelet shaped particles. Such shapes minimise the volume fraction at which the particles can form a connecting, percolating, conductive structure with each other and/or the dispersed, conductive emulsion phase.

In order to provide other properties required from wellbore fluids, the wellbore fluids of this invention may further contain any known wellbore fluid additives such as clay, organoclay, or polymeric viscosifiers, filtration reducers such as lignite derivatives, asphalts, asphaltites or polymers swollen by the NBL, weighting agents such as finely divided barytes or

hematite, lubricating additives, or any other functional additive known to those skilled in the art. These additives aim to provide a drilling mud that has the following characteristics :

- be fluid and produce affordable pressure drop in surface pipes and drill string
- have a yield stress suitable for supporting/transporting mud solids and drill cuttings
- 5 • be chemically, thermally and mechanically stable
- provide hole stability
- provide good lubricity
- prevent excessive fluid loss to the formation

The electrically conductive non-aqueous base of the present invention and the use thereof in drilling fluids is further illustrated.

The Polar Organic Liquid Component

The polar organic liquid POL component of the present invention exhibits a dielectric constant of at least about 5.0, and preferably of at least 10, and a Hildebrand solubility parameter of at least about $17 \text{ (J cm}^{-3})^{1/2}$ at 20 °C.

Polar organic liquids that exhibit low water-miscibility and higher oil-miscibility are generally preferred.

Said polar organic liquid POL may be compounds comprising at least one hydroxyl group selected for example from the following list :

- 20 • aliphatic and alicyclic alcohols of carbon numbers C_5 - C_{10} such as *n*-pentanol, cyclohexanol, *n*-octanol, 2-ethylhexanol, and *n*-decanol;
- phenols such as ortho-, meta-, or para-cresol;
- glycols such as 1,3-butane diol, 1,4-butane diol, 2-ethylhexane-1,3-diol;
- 25 • polyalkylene glycols such as polypropylene glycols of molecular weight above about 1000 (higher molecular weight leads to a oil-miscibility and lower water-miscibility), polybutylene glycols, polytetrahydrofuran, polyalkylene glycols or copolymers of ethylene oxide and/or propylene oxide and/or butylene oxide initiated by any hydroxylic or amino-functional moiety wherein the polyalkylene

glycol or copolymer is further characterised by exhibiting a cloud point (at 1% concentration in water) of less than about 10 °C;

- mono-alkyl or mono-aryl ethers of glycols or polyalkylene glycols such as ethylene glycol monobutyl ether, diethylene glycol monobutyl ether, dipropylene glycol monomethyl ether, tripropylene glycol monomethyl ether, propylene glycol monobutyl ether, dipropylene glycol monobutyl ether, tripropylene glycol monobutyl ether, propylene glycol phenyl ether, dipropylene glycol phenyl ether;
- diacetone alcohol (4-hydroxy-4-methyl-1,2-pentanone); acetylacetone; acetonylacetone and polyketones such as the copolymer of ethylene and carbon monoxide.

Another class of suitable compounds includes aprotic solvents having no proton that can be donated to a solute such as :

- methylisobutyl ketone, cyclohexanone, isophorone;
- dialkyl ethers of polyethylene glycols such as the dimethyl ethers of oligomers of ethylene glycol, the dimethyl ethers of polyethylene glycols such as PEG 400 or PEG 600 or PEG 1000, the dimethyl ethers of oligomers of propylene glycol or of polypropylene glycols;
- cyclic polyethers such as 1,4,7,10,13,16-hexaoxacyclooctadecane ([18] Crown-6);
- N-alkyl-2-pyrrolidones wherein the alkyl is of carbon number C₁-C₁₂, such as N-methyl-2-pyrrolidone, N-cyclohexyl-2-pyrrolidone, N-octyl-2-pyrrolidone, N-dodecyl-2-pyrrolidone;
- N-methylpiperidone;
- N,N-dialkyl alkanoamides such as dimethylformamide, dimethylacetamide, and higher homologues such as N,N-dimethyloctanoamide and N,N-dimethyloleamide;
- N,N,N',N'-tetramethylurea; dimethylsulphoxide; hexamethyl phosphoric triamide; 1,3-dimethyl-2-imidazolidinone; nitromethane or nitroethane; nitrobenzene; tetramethylene sulphone; γ -butyrolactone; and propylene carbonate.

The relationship between the relative permittivity, ϵ_r , thought to be measured at 10 kHz (for pure liquid the dielectric constant varies only at very high frequencies, i.e. 10⁵ Hz or higher) and 20 °C) and the Hildebrand solubility parameter is shown in the following tables I and II. Dielectric constant is the permittivity of the substance divided by the permittivity of vacuum.

Table I provides examples of material suitable for the present invention while table II shows examples of non-acceptable materials. To this aspect, it is worth noting that SHELLSOL D70, a product available from Shell Chemical Co-UK, may be considered as a typical mineral oil while the butyl oleate is a typical ester.

TABLE I			
Type	Compound	Relative permittivity ϵ_r	Solubility Parameter $(J\ cm^{-3})^{1/2}$
Alcohols	Methanol	31.2	29.7
	Propan-2-ol	18.6	23.5
	1-pentanol	13.9	22.3
	Diacetone alcohol	18.2	18.9
	n-octanol	10.3	21
Phenols	o-cresol	11.5	27.1
	m-cresol	11.8	27.1
	p-cresol	9.9	27.1
Aprotics	Dimethylformamide (DMF)	36.7	24.9
	Dimethylacetamide (DMAC)	37.8	22.1
	N-methyl-2-pyrrolidone (NMP)	32	23.1
	N-octyl-2-pyrrolidone		18.9
	N-dodecyl-2-pyrrolidone		18.2
	Dimethylsulfoxide (DMS)	48.9	24.5
	1,3-dimethyl-imidazolidinone	37.6 (1MHz)	
	Tetrahydrothiophene 1,1-dioxide (sulfolane or tetramethylene-sulfone)	43.3	
	Propylene Carbonate	64.92	27.2
	Hexamethylphosphoric triamide $O = P [N(CH_3)_2]_3$	29.3	
	Tetramethylurea	23	
	Nitrobenzene	35.7	
Ketone-type compounds	Diacetone alcohol (4-hydroxy-4-methyl-2-pentanone)		18.9
	Acetyl acetone	25	
	Methyl isobutyl ketone	13.1	17.2
	Isophorone		19.2
	Cyclohexanone	18.3	20.3
Glycols	1,2 propylene glycol	32	25.8
	1,3 butanediol		23.7
	Hexylene glycol (2-methyl-2,4-pentanediol)	7.7	23.1
Ethers	Ethylene glycol monobutylether (EGMBE)	9.4	18.4
	Dipropylene glycol mono- methyl ether	9	19.3
	Ethylene glycol mono- butyl ether	9.4	18.4

TABLE II Compound	Relative permittivity ϵ_r	Solubility Parameter (J cm⁻³)^{1/2}
<i>n</i> -pentane	1.84	
<i>n</i> -hexane		14.87
SHELLSOL D70(like mineral oil)	2.15	15.5
<i>n</i> -butyl acetate	5.1	17.6
Butyl oleate(like typical ester)	4	
Benzene	2.28	18.7

The Organic Liquid Component

The high-resistivity OL component can be crude oil, hydrocarbon refined fractions from crude oil such as diesel fuel or mineral oil, synthetic hydrocarbons such as *n*-paraffins, alpha-olefins, internal olefins, and poly-alphaolefins; synthetic liquids such as dialkyl ethers, alkyl alkanooate esters, acetals; and natural oils such as triglycerides including rape-seed oil, sunflower oil and mixtures thereof. Low toxicity and highly biodegradable oils will be generally preferred especially for offshore drilling.

The OL component may be present at up to 99.5% by volume of the NBL but formulations comprising up to 95% generally provides the better results.

The Dissolved Component.

The dissolved component DC is a conductivity enhancing component. It has to display sufficient solubility and current carrying abilities in the POL, the OL or the mixture of POL and OL. It has been found that different types of materials may be used :

- water if POL is used as part of the NBL
- some inorganic salts
- some organic bases
- quaternary ammonium salts or hydroxides

Inorganic salts

Suitable inorganic salts (including metal salts of partially organic acids such as methanesulphonic acid, toluenesulphonic acid) are characterised in that the anion of the salt is the conjugate base of an acid whose dissociation constant (pK_a) in water at 298 °K is less than about 1.0, and the cation is ammonium ion or a metal ion with an ionic radius which is less than about 2/3 of the ionic radius of the pre-selected anion.

The crystal ionic radii of typical cations and anions are shown table III.

Table III Cations*	Radius in Angstroms	Anions	Radius in Angstroms
NH ₄ ⁺	1.48	F ⁻	1.33
Li ⁺	0.68	Cl ⁻	1.81
Na ⁺	0.97	Br ⁻	1.96
K ⁺	1.33	I ⁻	2.20
Rb ⁺	1.47	SCN ⁻	<div style="text-align: center;"> ↓ INCREASING </div>
Cs ⁺	1.67	ClO ₄ ⁻	
Mg ²⁺	0.66	Methanesulphonate	
Ca ²⁺	0.99	Benzenesulphonate	
Sr ²⁺	1.12		
Al ³⁺	0.51		
Fe ³⁺	0.64		
Zn ²⁺	0.74		
Cu ²⁺	0.72		

* Some uncertainty depending on source

The ratio of ionic radii M^{n+} / A^{x-} is shown in table IV. Salts with ratio smaller than about 0.67 are generally acceptable, provided the dissociation constant (pK_a) in water at 298 °C of the acid providing the anion is less than about 1.0. LiF and MgF₂ are thus excluded on pK_a grounds.

Table IV : Ratio of cation/anion radius

Anions→	F ⁻	Cl ⁻	Br ⁻	I ⁻	SCN ⁻	ClO ₄ ⁻	CH ₃ SO ₃ ⁻	C ₆ H ₅ SO ₃ ⁻
Cations ↓								
NH ₄ ⁺	1.11	0.82	0.76	0.67		→ Decreasing →		
Li ⁺	(0.51*)	0.375	0.347	0.309		→ Decreasing →		
Na ⁺	0.73	0.536	0.495	0.441		→ Decreasing →		
K ⁺	1.00	0.735	0.679	0.605		→ Decreasing →		
Rb ⁺	1.11	0.81	0.75	0.668		→ Decreasing →		
Cs ⁺	1.26	0.92	0.85	0.76		→ Decreasing →		
Mg ²⁺	(0.49*)	0.36	0.34	0.30		→ Decreasing →		
Ca ²⁺	0.74	0.55	0.51	0.45		→ Decreasing →		
Sr ²⁺	0.84	0.62	0.57	0.51		→ Decreasing →		
Al ³⁺		0.28	0.26	0.23		→ Decreasing →		
Fe ³⁺		0.35	0.33	0.29		→ Decreasing →		
Zn ²⁺		0.41	0.38	0.34		→ Decreasing →		
Cu ²⁺		0.40	0.37	0.33		→ Decreasing →		

(*) = excluded on pK_a grounds

The pK_a values at 298 °K of certain acids providing anions useful (or not useful) in this invention are shown in table V :

Table V "Allowed" Anions	pK _a of Acid
INCLUDED:-	
Chloride	< -1
Bromide	< -1
Iodide	< -1
Thiocyanate	~1
Perchlorate	<< -1
Nitrate	-1.4
Trichloracetate	0.7
Benzene sulphonate	0.7
Toluene sulphonate	0.7
Naphthalene sulphonate	0.57
Picrate	0.38
Permanganate	<< -1
Methanesulphonic acid	-1
Trifluoromethanesulphonic acid	<<< -1
2,4-dinitrobenzenesulphonic acid	<< -1

EXCLUDED:	
Fluoride	3.45
Phosphate $O = P(OH)_3$ [steps 1,2 & 3]	2.12, 7.21, 12.67
Carbonate [steps 1 & 2]	6.37, 10.25
Acetate	4.75
Higher alkanoates	4.8 - 5.0
Dichloroacetic	1.48

For instance, the inorganic salt comprises anions which are the conjugate base of an acid selected from the class including hydrochloric acid; hydrobromic acid; hydroiodic acid; thiocyanic acid; perchloric acid; nitric acid; permanganic acid; sulphuric acid; alkane sulphonic acids such as methane sulphonic acid and ethane sulphonic acid; arene sulphonic acids such as benzene sulphonic acid, toluene sulphonic acid and naphthalene sulphonic acid; alkane and arene sulphonic acids substituted with electron-withdrawing groups such as trifluoromethane sulphonic acid and 2,4-dinitrobenzene sulphonic acid; picric acid and trichloroacetic acid. It is to be noted that phosphates, carbonates, alkanoates and fluorides are excluded.

Examples of suitable salts are :

- ammonium iodide, ammonium thiocyanate, ammonium trichloroacetate, ammonium methanesulphonate, and ammonium salts of higher molecular weight organosulphonic acids including halogeno-substituted or nitro-substituted sulphonic acids;
- potassium bromide, potassium perchlorate, potassium nitrate, potassium permanganate and potassium salts of the anions listed in this Claim for ammonium;
- sodium chloride and sodium salts of the other anions listed previously;
- any lithium salt of any of the anions listed previously;
- a salt formed from any of the anions listed previously with any of magnesium ion, calcium ion, and strontium ion;
- a salt formed from any of the anions listed in this Claim with any of the divalent cations of manganese, iron, cobalt, nickel, copper, or zinc;
- a salt formed from any of the anions mentioned before with the trivalent cations of iron or aluminium.

Organic bases

Another type of suitable material comprises of organic bases that are characterised by exhibiting a pK_a in water at 298 °K of more than 10.0.

pK_a data for some organic bases are shown in table VI

Table VI	
Compound	pK_a at 298 °K
Triethylamine	11.01
<i>n</i> -amylamine	10.6
<i>n</i> -decylamine	10.64
<i>n</i> -dodecylamine	10.63
Diethylene triamine (1 st ionisation)	10.1
Triethylene tetramine(1 st ionisation)	10.2
Piperidine	11.12
2,2,6,6-tetramethylpiperidine	11.07
Pyrrolidine	11.27
1,2-dimethylpyrrolidine	10.2
1,3-diaminopropane (1 st ionisation)	10.94
1,4-diaminobutane	11.15
Hexamethylene diamine	11.9

Examples of suitable organic bases are tri-alkylamines wherein the alkyl groups contain from 2 to 18 carbon atoms; piperidine; alkylpiperidines such as 1-ethylpiperidine and 2,2,6,6-tetramethylpiperidine; pyrrolidine; alkylpyrrolidines such as 1,2-dimethylpyrrolidine; ethyleneamines such as diethylene triamine, triethylenetetramine; N-alkylated ethyleneamines such as N,N,N',N'-tetramethylethylene diamine; alkylene diamines such as 1,3-diaminopropane, 1,4-diaminobutane and hexylene diamine; guanidine; N,N,N',N'-tetramethylguanidine.

Quaternary ammonium salts

A third type of dissolved component is a quaternary ammonium salt or hydroxide. Those include chlorides, bromides, iodides, methosulphates, ethosulphates or hydroxides of quaternary ammonium cations having alkyl and/or aryl and/or alkylaryl groups such that the total number of carbon atoms in all the groups combined with the nitrogen atom is in the range 8 to 60, and more preferably in the range 12 to 40. Examples include tetrabutyl

ammonium halides, tetraoctyl ammonium halides, dimethyldioctyl ammonium halides, methylbenzyldioctyl ammonium halides, tetradodecyl ammonium bromide.

N-Alkyl pyridinium salts or hydroxide

- 5 Another type of dissolved component is N-alkyl pyridinium salts or hydroxides that possess an alkyl, aryl, or alkylaryl group having between 6 and 24 carbon atoms combined with the nitrogen, and are provided as the chloride, bromide, iodide or hydroxide. An example is cetylpyridinium bromide.

10 **Examples of continuous liquid phase with enhanced electrical conductivity:**

An impedance analyser has been used to measure the electrical conductivity of various liquid samples over a range of frequencies from 5 Hz to 100 kHz. In the examples below, the measurements at 1 kHz and 10 kHz are given. The specific conductivity is in units of $\mu\text{S m}^{-1}$.

15 **Example 1.**

The conductivity of C_{14} - C_{16} linear α -olefin (LAO) as component OL was measured:

<u>Frequency (kHz)</u>	<u>Specific Conductivity ($\mu\text{S m}^{-1}$)</u>
1	0.03
10	0.28

20

Example 2.

The conductivity of LAO as OL containing 1.1% by weight of tetrabutylammonium bromide (TBAB) as component DC was measured:

<u>Frequency (kHz)</u>	<u>Specific Conductivity ($\mu\text{S m}^{-1}$)</u>
1	0.17
10	0.49

25

Example 3.

The conductivity of dipropylene glycol monomethyl ether (DPM, $\epsilon_r = 9$, solubility parameter = 19.3) as component POL was measured:

<u>Frequency (kHz)</u>	<u>Specific Conductivity ($\mu\text{S m}^{-1}$)</u>
1	57.6
10	59.3

Example 4.

The conductivity of mixtures of TBAB in DPM at 1, 2 and 5% by weight were measured:

	Specific conductivity ($\mu\text{S m}^{-1}$)		
<u>Frequency (kHz)</u>	<u>1% TBAB</u>	<u>2% TBAB</u>	<u>5% TBAB</u>
1	3.3×10^3	6.0×10^3	1.5×10^4
10	3.4×10^3	6.0×10^3	1.6×10^4

Example 5.

The conductivity of a mixture of LAO and DPM at 60/40 volume ratio, respectively, was measured:

<u>Frequency (kHz)</u>	<u>Specific Conductivity ($\mu\text{S m}^{-1}$)</u>
1	2.4
10	4.0

Example 6.

The conductivities of mixtures of LAO and DPM at 60/40 volume ratio, containing 1, 2 and 3% of dissolved component TBAB were measured:

	Specific conductivity ($\mu\text{S m}^{-1}$)		
<u>Frequency (kHz)</u>	<u>1% TBAB</u>	<u>2% TBAB</u>	<u>3 % TBAB</u>
1	2.1×10^2	2.9×10^3	3.4×10^3
10	2.1×10^2	2.9×10^3	3.6×10^3

Figure 1 shows the measured conductivity depending on the chosen frequency for the above mentioned OL, OL and POL at 60/40 ratio and OL and POL at 60/40 ratio containing 1, 2 and 3% of dissolved component DC. The above examples show that the beneficial use of components DPM and TBAB increases the electrical conductivity of component LAO by up to five orders of magnitude.

Example 7.

A 60/40 volume mixture of LAO/N-octyl-2-pyrrolidone (SURFADONE LP-100 available from GAF, USA) + 5% TBAB produced conductivity of $550 \mu\text{S m}^{-1}$ at 500 Hz.

Examples of drilling fluid with enhanced electrical conductivity:

Example 8.

The mixture of example 7 was used as the liquid phase of a drilling fluid according to the following formulation of density 10.5 lb/gal:

Example 7 Base Fluid	224.6 g
ULTIDRILL EMUL HT	5.0 g
INTERDRILL S	3.0 g
TRUVIS	8.0 g
LIME	2.0 g
BARITE	198.6 g

The conductivity of the above mud was $730 \mu\text{S m}^{-1}$.

Example 9.

The organic-water ratio of the mud of example 8 was reduced to 97/3 by adding the proportional amount of brine to produce a water activity of 0.75:

Example 7 Base Fluid	218.0 g
ULTIDRILL EMUL HT	5.0 g
INTERDRILL S	3.0 g
TRUVIS	8.0 g
LIME	2.0 g
CaCl ₂ (83.5%)	3.53 g
WATER	8.36 g
BARITE	193.3 g

The conductivity was measured to be $1200 \mu\text{S m}^{-1}$.

Example 10.

The organic-water ratio of the mud of example 8 was further reduced to 90/10 and the conductivity was measured to be $1,400 \mu\text{S m}^{-1}$.

Example 11.

The organic-water ratio of the mud of example 8 was further reduced to 60/40 and the conductivity increased to $3,400 \mu\text{S m}^{-1}$. The mud appeared stable but exhibited an electrical stability (ES) voltage of only 6 Volts.

Example 12.

A 77/23 volume mixture of N-octyl-2-pyrrolidone and dimethyloctanoamide (HALLCOMID M8-10 available from CP HALL, USA) was produced. To this was added 10% of TBAB.

The conductivity of this mixture was $15,000 \mu\text{S m}^{-1}$.

Example 13.

To 60 parts by volume of the mixture of example 12 was added 40 parts by volume of LAO. The conductivity of this mixture was $5,500 \mu\text{S m}^{-1}$.

Example 14.

The mixture of example 13 was used as the liquid phase of a drilling fluid with the following formulation (density 10.5 lb/gal):

Example 13 base Fluid	224.6 g
ULTIDRILL EMUL HT	5.0 g
INTERDRILL S	3.0 g
TRUVIS	8.0 g
LIME	2.0 g
BARITE	198.6 g

The measured conductivity of this fluid was $5,000 \mu\text{S m}^{-1}$.

Example 15.

The organic-water ratio of the formulation of example 14 was reduced to 95/5 by adding a proportional amount of brine (density 10.5 lb/gal ; water activity 0.75):

Example 13 Base Fluid	213.7 g
ULTIDRILL EMUL HT	5.0 g
INTERDRILL S	3.0 g
TRUVIS	8.0 g
LIME	2.0 g
CaCl ₂ (83.5%)	5.89 g
WATER	13.96 g
BARITE	189.7 g

The measured conductivity of this formulation was $8,100 \mu\text{S m}^{-1}$.

Example 16.

The oil-water ratio of the formulation of example 15 was further reduced to 70/30. The conductivity increased to $11,700 \mu\text{S m}^{-1}$. The mud appeared stable but exhibited an Electrical Stability value of 0 Volts.

Example 17

The plot of figure 2 shows the variation of conductivity with volume ratio of LAO to pyrrolidone-amide-salt mixture (defined in Example 12).

Example 18.

In this example, the mud was a 70/30 organic-water ratio invert emulsion- of density 10.5 lb/gal. The organic liquid (continuous phase) of this mud consisted of a 40/60 volume

mixture of LAO and a conductivity enhancing formulation. The conductivity enhancing formulation was as described in Example 12, except that the concentration of TBAB was 7.5%.

The brine phase was saturated sodium bromide with a specific gravity of 1.50. The water activity of the mud system was 0.58, measured at 22.5 °C. The prepared formulation is :

Components	Amount to make 350 ml
ORGANIC LIQUID	154.3g
ULTIDRILL EMUL HT	10.0 g
INTERDRILL S	3.0 g
TRUVIS	8.0 g
LIME	2.0g
NaBr brine	136.7g
BARITE	127.1 g

The drilling fluid was hot rolled at 250 °F (121 °C) for 16 hours and the rheological properties determined before and after hot rolling :

Parameter	Before Hot Rolling	After Hot Rolling
Fann Dial Reading @ 600 rpm	57	57
Fann Dial Reading @ 300 rpm	35	36
Fann Dial Reading @ 200 rpm	27	28
Fann Dial Reading @ 100 rpm	18	18
Fann Dial Reading @ 6 rpm	6	6
Fann Dial Reading @ 3 rpm	5	5
10 s gel strength (lb/100 sq ft)	5	8
10 m gel strength (lb/100 sq ft)	5	8
Apparent Viscosity (cps)	28 ½	28 ½
Plastic Viscosity (cps)	22	21
Yield Point (lb/100 sq ft)	13	15
Electrical Stability (V)	0	0
HTHP filtrate @ 250 °C, 500 psi (ml)		14

Conductivity Results (at 500 Hz and at room temperature):

	Before Hot Rolling	After Hot Rolling
Organic Liquid Phase	$0.9 \times 10^4 \mu\text{S m}^{-1}$	
Full mud	$1.4 \times 10^4 \mu\text{S m}^{-1}$	$1.45 \times 10^4 \mu\text{S m}^{-1}$
Filtercake		$1.3 \times 10^4 \mu\text{S m}^{-1}$
Filtrate (organic phase)		$0.4 \times 10^4 \mu\text{S m}^{-1}$

The conductivity of freshly made mud is about $14,000 \mu\text{S m}^{-1}$. This level is maintained through thermal aging at 250°F . The filtercake and filtrate also show increased conductivity. The conductivity additives do not have a deleterious effect on the rheology, both before and after thermal aging.

The volume of filtrate at 14 ml is an acceptable value for oil-based muds.

Shale dispersion inhibition

50 g of reactive cuttings (sized Oxford clay, 2-4 mm) was mixed in with 350 ml of the mud. The mixture was then rolled in an oven at 50°C for 2 hours. The weight loss occurring in the cuttings as a result of dispersion of the clay into the mud was then measured on a dry weight basis. For comparison with a water-based mud, a similar test was performed with a sea-water VISPLEX mud. VISPLEX II, mark of Schlumberger, is a mixed-metal hydroxide system. The results are:

Conductive OBM: ~0% dispersion

VISPLEX II: 10% dispersion

The conductive organic-based mud provided the shale dispersion inhibition typical of oil-based muds.

Example 19.

5% (w/w) of sodium bromide (NaBr) was added to a 70/30 volume mixture of ethoxylated lauryl alcohol and tripropyleneglycol methylether. The room temperature conductivity at 500Hz was $5000 \mu\text{S m}^{-1}$.

Example 20.

The solvent mixture of example 19 was used to produce an invert emulsion mud in which the volume ratio of Ultidrill base fluid to the solvent mixture was 60/40. The volume ratio of the total organic liquid phase to the aqueous phase was 90/10. The formulation is shown below:

ULTIDRILL base fluid	119.3 g	TRUFLO 100	3.75 g
Solvent mixture	96.3 g	TRUVIS HT	8.0 g
Sodium bromide	14.0 g	Lime	5.0 g
ULTIDRILL EMUL HT	10.0 g	Water	30.0 g
ULTIDRILL FL	3.5 g	Barite	151.3 g

- 5 The room temperature conductivity at 500Hz was $600 \mu\text{S m}^{-1}$.

Example 21.

10% (w/v) of lithium bromide (LiBr) was added to a 50/50 volume mixture of Ultidrill base fluid and dipropylene glycol *n*-butyl ether (DPnB). The room temperature conductivity at

- 10 500Hz was $7300 \mu\text{S m}^{-1}$.

Example 22.

An invert emulsion mud was produced in which the volume ratio of the organic phase to the aqueous phase was 95/5. The full formulation is shown below:

ULTIDRILL base fluid	48.23 g	TRUVIS HT	12.0 g
DPnB	195.8 g	LIME	5.0 g
LITHIUM BROMIDE	44.5 g	WATER	15.24g
ULTIDRILL EMUL HT	6.0 g	BARITE	152.9 g
INTERDRILL S	6.0 g		

- 15 The room temperature conductivity at 500 Hz was $9400 (\mu\text{S/m})$.